

TITLE OF THE INVENTION

DIRECT CURRENT VIBRATION MOTOR AND ARMATURE STRUCTURE

CROSS-REFERENCE TO RELATED APPLICATIONS

5 This application is based upon and claims the
benefit of priority from the prior Japanese Patent
Application No. 2000-027595, filed February 4, 2000,
the entire contents of which are incorporated herein by
reference.

BACKGROUND OF THE INVENTION

10 The present invention is applied to a direct
current vibration motor used in an incoming call
vibration-generating device for a mobile telephone or
the like. More particularly, the present invention
relates to a direct current vibration motor suitable
15 for a size reduction and an armature structure thereof.

As a flat-type direct current vibration motor used
in a small-size wireless telephone paging device and
a mobile telephone, for example, as shown in FIG. 15,
there is known a motor in which a rotor has an
20 eccentric structure (Jpn. Pat. Appln. KOKAI Publication
No. 6-205565). This vibration motor comprises a stator
102 comprising four permanent magnets 101 arranged in
a ring-like configuration and magnetized in an axial
direction, and a rotor 104 provided with an armature
25 103 located opposite to the permanent magnets 101 of
the stator 102, wherein the armature 103 of the rotor
104 is constituted in such a manner that the whole

armature 103 of the rotor 104 is formed in a fan-like configuration by allowing three coils 105 to which current is supplied to be located adjacent to each other in a circumferential direction with the result
5 that the rotor 104 is formed in an eccentric structure.

When current is supplied to these three coils 105 via a commutator 106, the rotation direction of the rotor 104 is determined by the Fleming's left hand law with the direction of the current and the
10 direction of the magnetic force from the permanent magnets 101. Current flowing via the commutator 106 is simultaneously supplied to two or more coils 105. At least two coils 105 out of the three coils 105 exceed the other coil 105 so that the restart-up
15 thereof is enabled irrespective of the suspension position of the rotor 104.

A vibration is generated with an eccentric load by the rotation of the rotor 104 by arranging the three coils 105 at an eccentric position deviated to one side
20 of the rotor 104 in this manner. With such three coil motors, even when the direction of the current flowing through the two coils are different, the start-up direction thereof can be made equal by arranging the three coils so that the direction of the magnetic force
25 corresponding to these coils becomes different. As a consequence, the motor can be started up irrespective of the suspension position of the rotor 104.

By the way, along with the prevalence of mobile
telephones, a direct current motor smaller in size than
the conventional type is desired so that the incoming
vibration of the mobile telephones on trains or the
5 like can be felt through a wrist watch or the like worn
at all times by men instead of the main body of the
mobile telephones. However, with the conventional
flat-type direct current vibration motor described
above, the rotors are concentrated at one location in
10 a circumferential direction, but three phases coils are
arranged in parallel in the circumferential direction
so that the rotors inevitably become large in the
circumferential direction to some extent and no large
eccentric effect can be obtained with the result that
15 the strength of vibration felt by men is limited.
Consequently, when an attempt is made to reduce the
size of the external diameter of the vibration motor of
this type so far commercially sold on the market, there
arises a problem in that the function of vibration
20 motor cannot be sufficiently attained.

Therefore, in order to obtain a higher eccentric
effect with the small-size motor, there is proposed
an eccentric direct current vibration motor in which
the armature 202 of the rotor 201 is constituted of
25 one or two coils 203, for example, as shown in FIG. 16
(Jpn. Pat. Appln. KOKAI Publication No. 10-336983).
In this motor, the commutator 203 is divided into four

in the circumferential direction so that the divided
bodies of the commutator located opposite to each other
are commonly connected. At the same time, both
the start end and the terminal end of the coil are
5 connected to the adjacent divided bodies of the
commutator respectively to supply the current to
the divided bodies of the commutator via a brush
arranged through 90°. When the rotor 201 is rotated,
the direction of the current flowing through the
10 coil 203 for each of the rotation angle is reversed,
the rotation of the rotor 201 is sustained with the
absorption and the repulsion action of the N/S poles
of the permanent magnet 101 and the magnetic force of
the coil 203.

15 However, one coil type motor is constituted in
a mechanism in which the adjacent divided bodies of
the commutator are instantly short circuited with
the brush in that the direction of the current flowing
through the coil 203 is changed over. In this case,
20 the short circuit of the power source is generated.
Consequently, there is provided a non-electrification
dead point in which the brush is not connected to any
of the commutator so that such short circuit of the
power source is not generated. By the way, in the case
25 where the rotor 201 is suspended with this dead point,
current does not flow through the coil 203 at the next
time of rotation so that the start-up is disabled.

Therefore, in order to secure the start-up by preventing the suspension of the rotor at this dead point, an iron pin 205 formed of a magnetic body is provided which regulates the static position at one part of the armature 202.

However, even when an attempt is made to regulate the start-up position with the iron pin, the presence of the iron pin itself constitutes a rotation load. In addition, when a contact friction resistance between the brush and the commutator exceeds a return force to a normal static position with a magnetic force between the iron pin and a permanent magnet with an increase in the contact friction resistance with the lapse of time, the rotor is suspended at the dead point in the end. Furthermore, when the iron pin is arranged so that a magnetic force sufficiently larger than the friction force can be obtained, the magnetic force of the coil which will start the rotor becomes weaker than the magnetic force between the iron pin and the permanent magnet this time with the result that the start-up incapability is induced. Consequently, there is a problem in that the setting of the pin of the magnetic body and the arrangement thereof are difficult in the method for regulating the rotor to the static position with the pin of the magnetic body.

BRIEF SUMMARY OF THE INVENTION

The present invention has been made to solve such

a problem, and an object of the invention is to provide a direct current vibration motor, and an armature structure thereof which can obtain a sufficient vibration and which do not generate the start-up incapability while attempting to further reduce the size thereof and reduce the weight thereof.

According to a first claim of the invention, there is provided a direct current vibration motor comprising:

10 a stator formed of a permanent magnet magnetized in an axial direction so as to have magnetic poles at a plurality of locations in a circumferential direction, the magnet having a ring-like configuration or being arranged in a ring-like configuration;

15 a rotor rotatably provided with respect to the stator and having an armature located opposite to the magnetized surface of the permanent magnet eccentrically fixed to the rotation shaft; and

current path formation means comprising
20 a commutator and a brush for forming a current path for supplying to the armature current whose polarity is subsequently reversed along with the rotation of the rotor;

wherein the armature is provided with a first coil
25 and a second coil arranged in such a manner that the spatial phase becomes equal to each other, and the current path formation means supplies the current

to the first coil and the second coil respectively by making the electric phase different from each other.

According to a sixteenth claim of the invention, there is provided an armature structure of a direct
5 current vibration motor wherein a rotor is rotatably provided with respect to a stator formed of a permanent magnet magnetized in an axial direction so as to have magnetic poles at a plurality of locations in the circumferential direction, the magnet having
10 a ring-like configuration and being arranged in a ring-like configuration, the armature located opposite to the magnetic pole of the surface of the permanent magnet of the rotor is eccentrically fixed to the rotation shaft and a current path for supplying to
15 the armature current whose polarity is subsequently reversed along with the rotation of the rotor is formed of current path formation means comprising the commutator and the brush, the structure comprising a first coil and a second coil arranged so that
20 the spatial phase becomes equal to each other;

wherein current is supplied to the first coil and the second coil respectively by making different the electric phase with the current path formation means.

Additional objects and advantages of the invention
25 will be set forth in the description which follows, and in part will be obvious from the description, or may be learned by practice of the invention. The objects

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and advantages of the invention may be realized and obtained by means of the instrumentalities and combinations particularly pointed out hereinafter.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING

5 The accompanying drawings, which are incorporated in and constitute a part of the specification, illustrate presently preferred embodiments of the invention, and together with the general description given above and the detailed description of the preferred embodiments given below, serve to explain the principles of the invention.

10 FIG. 1 is an exploded perspective view showing a direct current vibration motor according to a first embodiment of the present invention;

15 FIG. 2 is a plan view showing the direct current vibration motor according to the first embodiment of the invention;

20 FIGS. 3A and 3B are circuit diagrams showing the direct current vibration motor according to the first embodiment;

 FIG. 4 is a view showing a relationship between a generation torque and time of the direct current vibration motor according to the first embodiment;

25 FIGS. 5A through 5F are views for explaining the torque generation principle of the direct current vibration motor respectively;

 FIG. 6 is a plan view showing the direct current

vibration motor according to one variation of the first embodiment of the present invention;

FIG. 7 is a plan view showing the direct current vibration motor according to one variation of the first embodiment of the present invention;

FIG. 8 is an exploded perspective view showing the direct current vibration motor according to a second embodiment of the present invention;

FIG. 9 is a plan view showing the direct current vibration motor according to the second embodiment;

FIGS. 10A and 10B are circuit diagrams showing the direct current vibration motor according to the second embodiment;

FIG. 11 is a view showing a relationship between a generation torque and time of direct current vibration motor according to the second embodiment;

FIGS. 12A through 12F are views for explaining the torque generation principle of the direct current vibration motor respectively;

FIG. 13 is an exploded perspective view showing the direct current vibration motor according to a third embodiment of the present invention;

FIG. 14 is a plan view showing a direct current vibration motor according to a variation of the second embodiment;

FIG. 15 is a plan view showing a conventional three coil type direct current vibration motor; and

FIG. 16 is a plan view showing a conventional one coil type direct current vibration motor.

DETAILED DESCRIPTION OF THE INVENTION

Hereinafter, the present invention will be explained in detail by referring to the embodiments shown in the drawings.

FIG. 1 is an exploded perspective view showing a flat-type direct current vibration motor according to a first embodiment of the present invention, and FIG. 2 is a plan view thereof.

This direct current vibration motor is constituted in such a manner that the whole motor is formed into a flat cylindrical configuration with a stator 1, a rotor 2 rotatably attached to this stator 1, and a cylindrical cover 3 for sealing the rotor 2. The stator 1 comprises a disc-like plate 11, four permanent magnets 12 arranged in a ring-like configuration and magnetized in an axial direction so that the S pole and the N pole are alternately arranged on this plate 11, a support shaft 13 for supporting the rotor 2 which rises from the center of the plate 11, and two brushes 14 and 15 extending from a gap between adjacent permanent magnets in the circumferential direction toward the central portion of the plate 11 and arranged with the spatial phase of 90° . Furthermore, the rotor 2 comprises a rotation shaft 21 rotatably supported on the support

shaft 13, an armature 22 fixed in an eccentric state to one portion of this rotation shaft 21 in the circumferential direction, and a commutator 23 arranged on the outside circumference of the rotation shaft 21 and divided into six in the circumferential direction. The commutator 23 constitutes current path formation means together with the brushes 14 and 15. The armature 22 includes the first coil 24 (an outside coil) and the second coil 25 (an inside coil), a resin frame 27 for integrally supporting these coils 24 and 25, and a pin 28 of the magnetic body for position regulation described later.

For example, as shown in FIG. 3, the first coil 24 and the second coil 25 are star connected. The commutator 23 is constituted in such a manner that divided pieces located opposite to each other out of six divided pieces are connected to each other, and a pair of these divided pieces are connected to one end of the coil 24, one end of the second coil and the common end of the first coil 24 and the second coil 25. Current is supplied to this commutator 23 from the brushes 14 and 15 arranged with a spatial phase difference of 90° . The brushes 14 and 15 are subsequently connected to each one end of the first coil and the second coil 24 and 25 and the common end thereof. Consequently, as shown in FIG. 3A, the rotor 2 is rotated and one of the brushes 14

(or 15) is positioned at a boundary of the divided body of the commutator 23, the current flows in a path from the power source → the brush 14 → the commutator 23 → the first coil and the second coil 24 and 25 → the commutator 23 → the brush 15 → the grounding.

Furthermore, as shown in FIG. 3B, when the rotor 2 is rotated and the brushes 14 and 15 come into contact with each one of the divided body of the commutator 23 respectively, current flows in a path from the power source → the brush 14 → the commutator 23 → at least one of the first coil and the second coil 24 and 25 → the commutator 23 → the brush 15 → the grounding.

In this manner, according to the present invention, even when one of the brushes 14 and 15 is located at the central position of the adjacent divided pieces and the adjacent divided pieces are short circuited with the brushes 14 and 15, the short circuit of the power source short circuit is not generated because of the two coil style.

FIG. 4 is a torque waveform view for explaining the operation of this direct current motor, and a portion shown with the slanted line in FIG. 4 shows the current supply interval. As shown in FIG. 4, current is supplied to the first coil and the second coil 24 and 25 by making the electric phase different. The generation torque at the time when the current flows through the coil is determined with the position

relationship between the coil and the magnetic pole,
and the current value. However, when the first coil 24
and the second coil 25 have equal spatial phases, the
generation torque in the period in which current is
5 supplied is approximately equal to each other.

The position relationship between the rotor 2
denoted by symbols a through f in FIG. 4, and the
stator 1 is shown in correspondence to each other as
shown in FIGS. 5A through 5F. In an interval a, as
10 shown in FIG. 5A, current flows in the same direction
as the first coil 24 and the second coil 25. Since
the two coils 24 and 25 pass the position which equally
stretches over the two permanent magnets 12, the
largest torque is generated both in the coils 24
15 and 25.

At time b, as shown in FIG. 5B, current
continuously flows through the first coil 24, but the
current supply to the second coil 25 is severed.
Thereafter, in an interval c, as shown in FIG. 5C,
20 current flows through only the first coil 24, and the
rotor 2 is rotated with the torque generated only in
the first coil 24.

When time d comes, as shown in FIG. 5D, the
current supply to the first coil 24 is severed, and
25 the current supply to the second coil 25 is started.
However, at the time of the change-over, current is
instantly severed. Naturally, in the case where

the brushes 14 and 15 are simultaneously connected to the two divided pieces of the commutator 23, current is not instantly severed. In an interval e, as shown in FIG. 5E, current flows through only the second coil 25, and a rotation torque is continuously generated in a relation with the magnetic pole. At time f, current supply to the first coil 24 is started.

In this manner, with this direct current vibration motor, current flows almost continuously through one or more coils even when the armature 22 is set at any angle. When current flows through the first coil and the second coil 24 and 25, a rotation torque is generated in a definite direction in accordance with the Fleming's left hand law. When a third coil is separately provided, and the third coil is arranged coaxially with the first coil and the second coil 24 and 25, current flows through the third coil in a separate direction from the first coil and the second coil 24 and 25 so that the direction of the magnetic force becomes opposite to each other. Thus, it is assumed that the rotation load of the rotor 2 is generated. As seen in the motor of the present embodiment, current flows through the coils 24 and 25 only with respect to the portion of two phases out of three phases. The portion of the other one phase is omitted so that the rotation load described above is not generated, so that a smooth rotation is enabled.

When the rotor 2 is rotated, the armature 22 becomes eccentric with respect to the rotation shaft 21 so that the vibration is generated with the centrifugal force.

With this motor, even when the adjacent divided
5 pieces of the commutator 23 are short circuited,
the coils 24 and 25 are intervened between the power
sources without fail, the short circuit current does
not flow. Consequently, the interval between
the adjacent divided pieces can be made as short as
10 possible, and the dead point can be set to zero.
As a consequence, it is possible to prevent the
generation of a phenomenon in which current will not
flow at the time of the start-up and the star-up
incapability is generated.

15 However, when the first coil 24 and the second
coil 25 are suspended in the state in which the first
coil and the second coil 25 are located immediately
above the magnetic pole, the armature 22 can be rotated
in any direction, so that the rotation direction
20 becomes indefinite. Consequently, in this embodiment,
the position regulation pin 28 comprising a magnetic
body is provided on the armature 22 so as to project in
a circumferential direction. Consequently, since the
pin 28 moves by receiving the magnetic force between
25 the permanent magnet 12 and the permanent magnet 12,
the position of the armature 22 in the suspended state
is positioned at a position where one of the rotation

torques is received without fail as shown in FIG. 2. This position is a point d in FIG. 4 and is shown as FIG. 5D.

Incidentally, the present invention is not
5 limited to the above first embodiment. In the first embodiment, the first coil 24 is set as the outside coil, and the second coil 25 is set as the inside coil. For example, as shown in FIG. 6, the first coil 31 and the second coil 32 may be simultaneously formed of
10 a double winding, a rotation torque equal for both coils 31 and 32 is generated, and can be formed in the same manner as the formation of one winding coil so that the manufacturing process can be facilitated.

Furthermore, as means having the same function as
15 the pin 28 which serves as a static position regulating means shown in FIG. 6, as shown in FIG. 7, the pin 33 may be arranged with a little inclination along the direction of the magnetic force so that the pin 33 is overlapped with the position of the end of the rotation
20 direction of the first coil and the second coil 24 and 25. By doing so, the armature 22 can be made compact in size. Incidentally, in this case, the angle of the pin 33 may be determined to an appropriate angle in order to obtain a degree of a magnetic absorption
25 force which does not affect the static position and the rotation drive.

As has been described above, according to the

first direct current vibration motor and the armature structure of the present invention, the armature comprises the first coil and the second coil arranged in such a manner that the spatial phases are made equal and the armature is constituted in such a manner that current is supplied to at least one of the first coil and the second coil. Thus, the armature can be constituted apparently in the same manner as the one coil motor with the result that the eccentric effect can be heightened. Furthermore, since current always flows through the first coil and the second coil, no electric non-conductive area (the dead point) is provided and a smooth start-up is enabled.

FIG. 8 is an exploded perspective view showing a flat type direct current vibration motor according to the second embodiment of the present invention, and FIG. 9 is a plan view thereof.

This direct current vibration motor is different from the motor shown in FIG. 1 in the structure of the armature 41. The armature 22 includes a first coil 24 (an outside coil) and a second coil 25 (an inside coil) which are coaxially wound, and a third coil (a start-up coil) 26 arranged adjacently to the coils 24 and 25 in the circumferential direction and a resin frame 42 for integrally supporting these coils 24, 25 and 26.

For example, as shown in FIG. 10, the first coil 24, the second coil 25 and the third coil 26 are

star connected. The commutator 23 is such that divided
pieces located opposite to each other out of the six
divided pieces are connected to each other, and a pair
of divided pieces connected to each other is connected
5 to one end of the first coil 24, one end of the second
coil 25 and one end of the third coil 26 respectively.
The other ends of the coils 24, 25 and 26 are commonly
connected. Current is supplied from the brushes 14 and
15 arranged in a spatial phase difference of 90° with
10 respect to this commutator 23. The two brushes 14 and
15 are subsequently connected to the commutator 23
connected to each one end of the first to three coils
24, 25 and 26 along with the rotation of the rotor 2.
As a consequence, as shown in FIG. 10A, the rotor 2 is
15 rotated and one of the brushes 14 (or 15) is positioned
at a boundary of the divided body of the commutator 23,
current flows in a path from the power source \rightarrow the
brush 14 \rightarrow the commutator 23 \rightarrow the first through the
third coils 24, 25 and 26 \rightarrow the commutator 23 \rightarrow the
20 brush 15 \rightarrow the grounding. Furthermore, as shown in
FIG. 10B, when the rotor 2 is rotated and the brushes
14 and 15 come into contact with each one of the
divided bodies of the commutator 23, current flows in
a path from the power source \rightarrow the brush 14 \rightarrow the
25 commutator 23 \rightarrow at least two of the first through the
third coils 24, 25 and 26 \rightarrow the commutator 23 \rightarrow the
brush 15 \rightarrow the grounding. In this manner, according

to the present invention, one of the brushes 14 and 15 is located at an intermediate position of the adjacent divided pieces. Thus even when the adjacent two divided pieces of the commutator 23 are short circuited, no power source short circuit is generated because of the three coil style.

FIG. 11 is a torque waveform view for explaining an operation of this direct current vibration motor, and a portion shown with the slanted line in FIG. 11 shows the current supply interval. As shown in FIG. 11, current is supplied to the first to the third coils 24, 25 and 26 by, for example, making different the electric phase. The generation torque at the time when current flows through the coil is determined with the position relationship between the coil and the magnetic pole position, and the current value. Since the first coil 24 and the second coil 25 have an equal spatial phases, the generation torque is approximately equal in a period in which current is supplied.

The position relationship between the rotor 2 and the stator 1 shown in a through f are shown in correspondence to each other in FIGS. 12A through 12F. In the interval a, as shown in FIG. 12A, current flows from the power source → the brush 14 → the commutator 23 → from the inside to the outside of the second coil 25 (in the clockwise direction) → from the inside to the outside of the first coil 24 (in the clockwise

direction) → the commutator 23 → the grounding.
Since the first coil and the second coil 24 and 25
passes through the position which equally stretches
over the two permanent magnets in the state in which
5 the current in the same direction flows, the largest
torque is generated both in the first coil and the
second coil 24 and 25.

At time b, as shown in FIG. 12B, the brush 14
connected to the power source is located at a boundary
10 between the commutator 23 connected to the inside end
of the second coil 25 and the commutator 23 connected
to the outside end of the third coil 26 so that current
begins to flow from the outside to the inside of
the third coil 26 (in an anticlockwise direction).
15 Thus, current instantly flows through the three
coils 24 through 26. Immediately after that, current
supply to the second coil 25 is severed. After that,
in the interval c, as shown in FIG. 12C, current flows
through the first coil 24 and the third coil 26, so
20 that the rotor 2 is rotated with the torque generated
in the first coil 24 and the third coil 26.

When time d comes, as shown in FIG. 12D, the
brush 15 connected to the grounding is positioned at
a boundary between the commutator 23 connected to the
25 outside end of the first coil 24 and the commutator 23
connected to the inside end of the second coil 25 with
the result that current supply to the second coil 25 is

started. However, current flows in a direction
opposite to the direction of the current which flows
through the first coil 24, so that current is severed
which flows through the first coil 24 immediately after
5 that. At this time, the first coil 24 and the second
coil 25 are located at a position just opposite to
the permanent magnet 12. Torque is not generated with
the first coil and the second coil 24 and 25. However,
current continues to flow through the third coil 26, so
10 that the largest torque is generated. In the interval
e, as shown in FIG. 12E, current flows between the
second coil 25 and the third coil 26, so that the
rotation torque is continuously generated in a relation
with the next magnet. At time f, the current supply to
15 the first coil 24 is started. Immediately after that,
the current supply to the third coil 26 is severed.
Current continues to flow through the second coil 25.

In this manner, in this direct current motor, even
when the armature 41 is set to any angle, current flows
20 almost continuously through two or more coils. When
current flows through the first through three coils 24,
25 and 25, a rotation torque in a definite direction is
generated in accordance with the Fleming's left hand
law. When the third coil 26 is coaxially arranged with
25 the first coil and the second coil 24 and 25, current
flows through the third coil 26 in a direction
different from the first coil and the second coil 24

and 25. Thus, the direction of the magnetic force becomes opposite, so that the rotation load of the rotor 2 is generated. Furthermore, as shown in FIG. 12D, at a position where the coils 24 and 25 are located opposite to the magnets, no torque is generated in any of the coils. When the motor is suspended at this position, it is assumed that the start-up incapability is generated. However, as seen in this embodiment, only two coils 24 and 25 out of the three coils are coaxially arranged, while the remaining coil is arranged so that the spatial phase becomes different from the counterpart of the former two coils. Thus, no rotation load is generated. Furthermore, even when the rotor 21 is suspended at the position of FIG. 12D, a smooth start-up is enabled with the third coil 26. In order to start up the motor efficiently, as shown in FIG. 9, it is desired that the spatial phase between the first coil and the second coil 24 and 25 and the third coil 26 is set to 135° or more as shown in FIG. 9.

When the rotor 2 is rotated, the armature 41 becomes eccentric with respect to the rotor 21. Consequently a vibration is generated with the centrifugal force. Since the two coils 24 and 25 are arranged by gathering the two coils 24 and 25 at one location in the circumferential direction in this motor, so that a high eccentric effect can be obtained.

Furthermore, since this motor is of three coil type, no short circuit current flows because at least two of the coils 24, 25 and 26 intervene between the power sources without fail even when the adjacent
5 divided pieces of the commutator 23 are short circuited via the brushes 14 and 15. That is, in the case of one coil type, it sometimes happen that a short circuit current flows between the power and the grounding via two phases where no coils happen to be present.
10 Consequently, in the case of one coil type, it is required to widen to some extent an interval between adjacent divided pieces in the circumferential direction so that no circuit is generated between adjacent divided pieces of the commutator 23 with the
15 brushes 14 and 15. Consequently, there arises a dead point where no current flows. With respect to this point, in this embodiment, no short circuit current flows between the power source and the grounding even when the adjacent divided pieces are short circuited.
20 Consequently, the interval between the adjacent divided pieces can be made as short as possible, so that the dead point where no current flows can be set to zero. As a consequence, it is possible to prevent the phenomenon in which no current flows at the time of the
25 start-up and the start-up incapability is generated.

FIG. 13 is an exploded perspective view showing a flat-type direct current vibration motor according to

different. The armature can be constituted ostensibly in the same manner as the two coils motor, so that the eccentric effect can be heightened as compared with the three coils motor. Furthermore, according to the present invention, current is supplied to the three coils so that the electric phase becomes different. Thus, no electric non-electrification interval (a dead point) is present, and a secured start-up is constantly started up. Furthermore, according to the present invention, current is supplied to the three coils so that the electric phase becomes different. No electric non-conductive interval (the dead point) is present, so that the secured start-up is enabled at all times. Furthermore, the motor comprises the first coil and the second coil and the third coil adjacent in the rotation direction, so that a space can be secured where the weight can be arranged which can enlarge the vibration in within the circumference. Besides, the countermeasure against the increase in the vibration amount as the vibration motor is favorable as well.

Incidentally, the present invention is not limited to the above embodiment. In the above embodiment, the first coil 24 is formed of an outside winding, and the second winding is formed of an inside winding. For example, as shown in FIG. 14, the first coil and the second coil 31 and 32 may be simultaneously formed of the double winding. When the first coil and

the second coil 31 and 31 are formed of the double
winding in this manner, a rotation torque equal to
both coils 31 and 32 is generated, and can be formed in
the same manner as the formation of one winding coil
5 with the result that the manufacturing process can be
simplified.

Additional advantages and modifications will
readily occur to those skilled in the art. Therefore,
the invention in its broader aspects is not limited to
10 the specific details and representative embodiments
shown and described herein. Accordingly, various
modifications may be made without departing from the
spirit or scope of the general inventive concept as
defined by the appended claims and their equivalents.